Optimal design of hydroelectric projects in Uttara Kannada, India

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Abstract The planning of water resources depends on the type and size of projects, the ecological factors involved, etc. Emphasis is placed on presenting an overview of water resources through meteorological, hydrological, ecological and economic data. Economic data include all costs and benefits, specifically those hitherto under estimated, environmental social costs and benefits. This study was carried out on the Bedthi and Aghnashini rivers in the Uttara Kannada district of the Western Ghats region, Karnataka State, India. It is estimated that 720 and 510 million kWh of electricity can be generated in Bedthi and Aghnashini River basins, respectively. If all the streams are harnessed, focusing on land submergence impact, a model is proposed to minimize submergence and maximize net energy in a region with seasonal power generation, reservoir storage capacity (to meet the region’s demand during all seasons) and installed generation capacity as the decision variables. Net energy analyses incorporating biomass energy lost in submergence show that maximization in net energy at a site is possible if the hydroelectric generation capacity is adjusted according to the seasonal variations in the river’s water discharge. A Decision Support System (DSS) used for optimal design of hydroelectric projects in Uttara Kannada district is discussed.

INTRODUCTION

Karnataka state has the unique distinction of having set up the first hydropower plant in India at Shivanasamudram in 1942. Since then, hydroelectric plants have contributed significantly to both the State’s and national demand for electricity. Most of Karnataka’s hydroelectric plants are located in Uttara Kannada district. Construction of
large reservoirs is restricted due to environmental constraints, necessitating the development of ecologically sound alternatives.

Hydroelectric power development—present status and approaches in design

At present hydroelectric power development is undertaken on an ad hoc, project-by-project basis with capacity based on 90% availability of water annually, estimated on the basis of a 10-day period. Since seasonal and yearly fluctuations of rainfall/streamflow are high, planners tend to opt for large reservoirs to achieve their goal. There is a need to consider integrated systems planning of supply and demand for optimal development of the potential considering 90% reliability of the system in the region. Demands of appropriate benefit-cost ratio (e.g., greater than 1.5), or least cost of generation for clearance, ignore the energy/economic costs of submergence and alternative designs involving seasonal variation in generation. Optimization (programming) and descriptive (predictive) model approaches are usually adopted to accomplish this complicated task (Falkenmark, 1989). Decision Support Systems (DSS) focus more on providing flexible tools for policy analysis than on providing models to answer structured problems (Parker & UI-Ataibi, 1986). This paper focuses on the design of a hydroelectric project using DSS, emphasizing economic efficiency and engineering soundness, subject to social, environmental, ecological, cultural, institutional and legal constraints.

OBJECTIVE

The objective is to design a hydroelectric plant utilizing optimal energy in the water, with minimum submergence and economic costs, considering seasonal variation in power generation to meet the region’s demand during all seasons.

STUDY AREA

Uttara Kannada district lies between 74°9’–75°10’E longitude and 13°55’–15°31’N latitude with 67% of its area under forest, 27% under habitation and reservoirs, and the rest under various cultivation covering 10,291 km² (Fig 1). The large reservoirs for hydroelectricity generation of Kali and Sharavathi have submerged vast tracts of natural forest and dislodged a large number of people. Therefore, an attempt is made to explore ecologically sound means of harnessing the hydroenergy of the Bedthi and Aghnashini rivers.

STREAMFLOW MEASUREMENT AND COMPUTATION OF POWER

Streamflow depends on drainage efficiency of hill slopes, moisture content of the soil, subsurface geology and vegetation cover (Gordon et al., 1992). Streamgauging using a current meter indicates that streams in these catchments are seasonal. The relationship between runoff at gauged sites and rainfall was determined by regression analysis. This relationship was used to assess the potential of ungauged streams. It was estimated that
about 720 and 510 million kWh of electricity could be generated in Bedthi and Aghanashini River basins, respectively.

The potential assessment shows that most of the streams would cater to the needs of local people in a decentralized way during the monsoon, ensuring continuous power supply, which would otherwise be disrupted by dislocation of electric poles/pylons or falling of trees/braches on transmission lines due to heavy winds. A detailed household survey of villages in hilly areas shows that people have to spend at least 60–65% of the season without electricity when depending on a centralized supply. In view of this, an ecologically sound alternative is proposed, which would generate maximum electricity during the monsoon season and sufficient electricity during the “lean” season.

DESIGN OF A RESERVOIR WITH ENERGY AND ECOLOGICAL CONSTRAINTS

The environmental impacts associated with large reservoirs necessitate the design of reservoirs of appropriate sizes to meet the target demand of a region (Mutreja, 1976).
Because of the negative aspects of hydroelectric projects in ecologically fragile hilly terrain; the submergence area should be minimized; the project should be subject to reasonable cost, minimum or no wastage of water and seasonal constraints (the region receives maximum rainfall during southwest monsoon). Based on 90 years’ precipitation data and 18 months of river runoff data, a methodology is proposed to design a storage reservoir at Magod to meet the region's demand during all seasons.

Hydroelectric energy operation module

A decision support system for optimal design and operation of a large network of small reservoirs for agriculture is described elsewhere (Labadie, et al., 1988; Albuquerque, 1993) The operation module is designed based on predetermined hydrological flow (database, environmental and socio-economic modules), a GIS module, technical data, economic data and a certain user selected reliability level. It also generates adaptive operation policies based on this reliability level. An adaptive optimum control module decides the quantity of water to be drawn from the reservoir considering seasonal constraints, volume of water stored for particular height of dam, seepage loss, evaporation loss, dead storage capacity of dam and rate of sedimentation, to ensure there is no wastage of water. It also decides the storage capacity during the non-monsoon season. The net energy available in the region is also presented in this module. Figure 2 shows the components of the planning operation module.

Design assumptions and parameters

Assumptions Detailed geological and topographical investigations carried out by the Department of Mines and Geology (KPCI, 1993) to determine the best site for the dam, pressure shaft alignment, powerhouse location, etc., can be used for implementing this design.

Parameters Input data consist of site specific data (discharge, water yield, generation head, evaporation rate, seepage rate etc.), technical data (efficiency of turbine and generator, and dependability norm for storage capacity, load factor, etc.) and economic
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...data (civil construction costs for various types and heights of dam, cost of electrical machinery of various capacities, environmental costs, rehabilitation costs, etc.).

**Decision variables** The decision variables determine the optimum storage capacity, installed generation capacity and seasonal power drafts; net energy availability in the region (objective function) needs to be maximized subject to seasonal hydrological constraints, and costs and submergence area are to be minimized.

**NET ENERGY MODEL—PARAMETRIC OPTIMIZATION**

The broad outline of an optimization model for exploiting a river for hydropower and irrigation, incorporating energy cost and net increase in yield due to irrigation, with constraints on arable area and crop water requirement and seasonal variation in precipitation, has been formulated by Subramanian (1985). On the same lines, with detailed engineering design and quantification of data, the parametric optimization approach is used with an objective to maximize the net energy subject to ecological constraints, given by:

\[ E_{net} = E_h - E_{bio} \]  

(1)

where \( E_{net} \) is net energy, \( E_h \) is hydroenergy and \( E_{bio} \) is bioenergy. This model is solved for various scenarios for optimal utilization of hydropower and thermal energy in the region. This includes an equation which computes monthly hydropower production as a function of volume of water discharged \( (Q) \), gross head of this water \( (H) \) and efficiency of the couple turbine generator \( (\eta_h) \), (between 0.7 and 0.85).

Hydropower (kW) is given by:

\[ P = 9.81 \cdot Q \cdot H \]  

(2)

The corresponding approximate electricity produced \( E_h = P \cdot t \cdot \eta_h \), where \( E_h \) is electricity (kWh) and \( t \) is operating time. The monthly hydroelectricity generated in million kWh is given by:

\[ E_{ht} = \sum 9.81D_i \cdot H \cdot \eta \]  

(3)

where \( i = 1, \ldots, 12 \) and \( D_i \) is the power draft from the reservoir during a month (million cubic meters, Mm³). Replacing 9.81 \( H \cdot \eta \) as constant \( k_h \):

\[ E_{ht} = \sum k_h \cdot D_i \]

This is decomposed for seasonal drafts:

\[ E_{ht} = \sum k_1 \cdot D_{sm} + \sum k_1 \cdot D_{sd} \]  

(4)

where \( D_{sm} \) and \( D_{sd} \) are water drawn during monsoon \( (m = 1, \ldots, 4) \) and dry period \( (d = 5, \ldots, 12) \), respectively.

Energy loss due to submergence is given by:

\[ E_{bio} = A_{sub} \cdot Gr \cdot (CV) \cdot \eta_s \]  

(5)

where \( A_{sub} \) is the submerged area classified on the basis of land use, \( Gr \) is the annual...
rate of growth or productivity, $\eta_c$ is energy conversion efficiency and $CV$ is the energy equivalence factor in terms of primary energy content (e.g. a ton of dry fuelwood with a calorific value of 4400 kcal kg$^{-1}$ has a thermal content of 5112.8 kWh).

This model is subject to the following constraints:

**Hydrological constraints** These operate on a monthly basis and consist mainly of the following continuity equation (Maass et al., 1962):

$$V_{t+1} = V_t + I_t - S_t - E_t - D_t$$  \hspace{1cm} (6)

where $V_t$ is the volume of the reservoir at the beginning of month $t$, $I_t$ is inflow to the reservoir, $S_t$ is seepage loss, $E_t$ is evaporation loss, and $D_t$ is discharge from the reservoir during the month $t$. Equation (6) is solved using inputs such as the functional relationship between surface area, seepage, evaporation vs volume, sequence of monthly inflows into the reservoir and policy for determining the discharges from the reservoir. A certain amount of “dead” storage capacity was added to account for sedimentation.

**Dependability** The storage capacity ($V$) of any reservoir is the function of both targeted draft ($D$) and reliability ($R$), given by:

$$V = f(D,R)$$  \hspace{1cm} (7)

It is seen that the required reliability of targeted draft has a direct relation to effective storage capacity, which has to be provided. For a given draft, particularly the one approaching a mean flow, the required storage is extremely sensitive to reliability. Similarly for a given level of reliability, increase in targeted draft would result in large storage. Thus, for a given draft, storage would increase substantially with increased reliability levels. For hydropower planning, in the case of power generation schemes, a dependability criterion of 90% on a yearly basis is normally adopted.

**Constraint on seasonal variation in generation capacity** If no variation is allowed:

$$P_{sm} = P_{sd}$$  \hspace{1cm} (8)

Allowing seasonal variation:

$$P_{sm} \geq P_{sd}$$  \hspace{1cm} (9)

If variation of “$r$” is allowed:

$$P_{sm} \geq rP_{sd}$$  \hspace{1cm} (10)

The variables $P_{sm}$ and $P_{sd}$ are hydroelectric generation capacity during monsoon and dry months, respectively, written in terms of power draft as:

$$P_{sm} = k_1 D_{sm}/LF_{sm}$$  \hspace{1cm} (11)

and

$$P_{sd} = k_1 D_{sd}/LF_{sd}$$  \hspace{1cm} (12)

where $LF_{sm}$ and $LF_{sd}$ are average load factors during monsoon and dry months, respectively. Therefore:
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\[
D_{\text{rel}}/LF_{\text{rel}} = D_{\text{rel}}/LF_{\text{rel}}
\]

\[
D_{\text{rel}}/LF_{\text{rel}} \geq r \cdot D_{\text{rel}}/LF_{\text{rel}}
\]

Assuming

\[
LF_{\text{rel}} = LF_{\text{rel}} \text{ (as 0.5)}
\]

Equations (13) and (14) would become

\[
D_{\text{rel}} = D_{\text{rel}}
\]

and

\[
D_{\text{rel}} \geq r \cdot D_{\text{rel}} \quad r = 1, 2, \ldots, \infty
\]

**Constraint on minimum storage**

\[
Ka \geq V_t \text{ for } t = 1, 2, \ldots, 12
\]

where \( Ka \) is the active storage capacity.

**Operating policy of the reservoir**

The feasible operating policy, considering seasonal variation in water inflow, would be: \( (SI \cdot P_{\text{rms}} + S2 \cdot P_{\text{med}}) \) 30 24 LF (amount of water/million kWh) = total quantity of water (in Mm\(^3\)) available at site. The load factor, LF is the ratio of average load to peak load.

From equations (12) and (15), with \( S1 = 4 \) (monsoon) and \( S2 = 8 \) (lean season) this constraint reduces to:

\[
4D_{\text{rel}} + 8D_{\text{rel}} = V_{t+1}
\]

The regulation through storage could be shown as follows:

If \( V_i + I_i - S_i - E_i - D_i \leq V_i \)

then

\[
D_i = V_i + I_i - S_i - E_i
\]

and

If \( V_i + I_i - S_i - E_i - D_i \geq V_i \)

then

\[
D_i + d = V_i + I_i - S_i - E_i
\]

where \( V_i \) is the storage volume of the reservoir and \( d \) the excess quantity available for generation.

**Positivity constraints**

Decision variables are positive

\[
D_i \geq 0 \text{ for all } t = 1, 2, \ldots, 12
\]

and

\[
V_i \geq 0 \text{ for all } t = 1, 2, \ldots, 12
\]

Therefore

\[
Ka \geq 0
\]
CASE STUDY

This design is implemented for the hydroelectric scheme at Magod

River discharge

The average annual yield at Magod is 1105 Mm$^3$ measured by empirical method. The 90% dependable water yield is estimated as 995 Mm$^3$. Water yield computed with 90 years precipitation data, shows that water quantity varies from $0.25 \pm 1.25$ during January to $364 \pm 136$ during July.

Evaporation, seepage loss and silting capacity

Evaporation and seepage losses for the region are estimated as 99 Mm$^3$ year$^{-1}$ for 100 km$^2$. The silt rate per annum is given by $S = C(A)^{0.4} = 4.25$ (where $C$ is the catchment coefficient and $A$ is the catchment area (in m$^2$)) assumed for a basin with plain and forested tracts. With the silt rate of 0.83 Mm$^3$ year$^{-1}$, the life of the reservoir at FRI 450–455 m is about 50 years.

Dam site

The site proposed 0.91 km upstream of Magod Falls, at longitude 74°45'28"E and latitude 14°51'41"N commands a basin area of 2084 km$^2$ and has exposed rocky bed at either side. The river bed level here is 373 m and it is 36 m wide.

Dam height and submergence area

When the water head is very high and given the reservoir profile—a deep valley with steep walls, hydroelectric energy becomes very competitive compared to bio-energy. When the water head is lower and the terrain has a slope less than 25°, the smaller reservoir depths and smaller submergence area make firewood an attractive option. A dam at this site would submerge areas having bioresources such as firewood, that are used for domestic, commercial and other purposes.

The volume of water stored for a particular dam height, computed by assuming the volume between two consecutive contours to be trapezoidal, is:

$$V_{12} = (a_1 + a_2) \cdot 0.5 \cdot h_{12} \tag{25}$$

where $V_{12}$ is the volume between contours 1 and 2, $a_1$ and $a_2$ are the area of contours 1 and 2 respectively, and $h_{12}$ is the height difference between contours 1 and 2. The generalized form could be written as:

$$V_i = \sum_{k=1}^{i-1} V_{j+k+1} \quad i = 1, j = i+1, i+2, \tag{26}$$
The submergence area, $A_{sub}$, and corresponding volume computed for different dam heights at Magod are depicted in Fig 3. This shows that when the dam height, $H_{dam}$ is 67 m, the submergence area is 5.7 km$^2$ and the volume is 106.35 Mm$^3$. Beyond 87 m, there is a steep increase in submergence area, as is evident from submergence area of 95.03 km$^2$ for dam height of 107 m. The relationship between submergence area and height of the dam is exponential ($A_{sub} = 0.38 e^{0.044 H_{dam}}$) with $r = 0.99$ and percentage error = 0.45. Similarly, the probable relationship between volume of water, $V_{dam}$, and height of the dam is exponential ($V_{dam} = 5.03 e^{0.054 H_{dam}}$) with $r = 0.99$ and percentage error = 0.22. This relationship between volume and height (actual and predicted), for Magod, is shown in Fig 4.

NET ENERGY ANALYSIS

Hydropower at each site has been computed before maximizing the net energy function. Energy from water is computed based on parametric optimization techniques, listed in Table 1. If variation is allowed between $P_m$ and $P_d$ (equations (8)-(12)), it reduces the storage capacity requirements. Figure 5 shows a graph of submerged area (in km$^2$) vs hydroelectricity generated. $E_h$. Regression analysis of these variables gives a hyperbolic relationship. More hydroelectric energy is harnessed by drawing the water during monsoon on a run-of-river basis and sufficient quantity is stored to meet the non monsoon requirement. By allowing a $P_m$ to $P_d$ ratio of 3, the submergence area saved is about 69.97% with an increase in electrical energy. This is because, for smaller heights of the dam, the submergence area is smaller and therefore evaporation and seepage losses are also lower. This saved area would also meet the bio-resource requirement of the region.
Fig. 4 Storage volume for various heights of dam at Magod

<table>
<thead>
<tr>
<th>Height (m)</th>
<th>Contour (m)</th>
<th>Sub-area (km²)</th>
<th>Volume (million Mm³)</th>
<th>Hydropower: $P_1/P_2$</th>
<th>$P_1$ (MW)</th>
<th>$P_2$ (MW)</th>
<th>Energy (million kWh)</th>
</tr>
</thead>
<tbody>
<tr>
<td>107</td>
<td>480</td>
<td>95.03</td>
<td>1736.35</td>
<td>1.00</td>
<td>85.00</td>
<td>85.00</td>
<td>746.66</td>
</tr>
<tr>
<td>97</td>
<td>470</td>
<td>63.23</td>
<td>1134.53</td>
<td>1.00</td>
<td>90.00</td>
<td>90.00</td>
<td>790.55</td>
</tr>
<tr>
<td>87</td>
<td>460</td>
<td>28.59</td>
<td>545.36</td>
<td>3.00</td>
<td>157.51</td>
<td>52.30</td>
<td>768.65</td>
</tr>
<tr>
<td>87</td>
<td>460</td>
<td>28.59</td>
<td>545.36</td>
<td>4.00</td>
<td>138.04</td>
<td>34.51</td>
<td>768.65</td>
</tr>
<tr>
<td>87</td>
<td>460</td>
<td>28.59</td>
<td>545.36</td>
<td>6.00</td>
<td>199.82</td>
<td>33.30</td>
<td>780.08</td>
</tr>
<tr>
<td>82</td>
<td>455</td>
<td>20.77</td>
<td>416.61</td>
<td>6.00</td>
<td>203.98</td>
<td>34.00</td>
<td>796.36</td>
</tr>
<tr>
<td>82</td>
<td>455</td>
<td>20.77</td>
<td>416.61</td>
<td>4.00</td>
<td>180.00</td>
<td>45.00</td>
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<td>3.00</td>
<td>163.37</td>
<td>54.46</td>
<td>796.27</td>
</tr>
<tr>
<td>77</td>
<td>450</td>
<td>16.27</td>
<td>416.61</td>
<td>6.00</td>
<td>210.00</td>
<td>35.00</td>
<td>819.87</td>
</tr>
<tr>
<td>77</td>
<td>450</td>
<td>16.27</td>
<td>416.61</td>
<td>4.00</td>
<td>184.63</td>
<td>46.16</td>
<td>810.90</td>
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<tr>
<td>77</td>
<td>450</td>
<td>16.27</td>
<td>416.61</td>
<td>3.00</td>
<td>166.15</td>
<td>55.38</td>
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</tr>
<tr>
<td>72</td>
<td>445</td>
<td>12.74</td>
<td>243.12</td>
<td>10.00</td>
<td>250.03</td>
<td>25.00</td>
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<td>70</td>
<td>443</td>
<td>9.98</td>
<td>185.72</td>
<td>8.00</td>
<td>200.02</td>
<td>20.00</td>
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<tr>
<td>67</td>
<td>440</td>
<td>5.70</td>
<td>106.35</td>
<td>8.00</td>
<td>159.98</td>
<td>10.00</td>
<td>823.55</td>
</tr>
</tbody>
</table>

Note: for dam heights of 72, 70 and 67 m, multiple $P_1/P_2$ ratios are possible

Biomass energy from lands to be submerged

The land-use pattern for various heights of dam shows area under natural forest as the major constituent, consisting of evergreen, semi-evergreen and deciduous forests. The primary production of biomass is estimated to range between 6.5–27.5 t ha$^{-1}$ year$^{-1}$
Fig 5 Energy generated vs submergence area

(Ramachandra, in press) Areca and coconut residues from gardens are in the range of 3–4.5 t ha\(^{-1}\) year\(^{-1}\). Considering the lower productivity of 6.5 t ha\(^{-1}\) year\(^{-1}\), the dam at Magod with a height of 107 m submerges about 95.03 km\(^2\), of which 88.53 km\(^2\) is under evergreen and semi-evergreen forests, rich in biodiversity and worth 34.21 MW in biomass (thermal) energy. A reduction in dam height to 67 m brings this value down to 1.93 MW, due to the decrease in the submergence area.

The net energy computed (Table 2), considering thermal value of bioresidues, indicates that, with decrease in dam height, the net available energy increases. At Magod, the net energy increases from 416.89 (dam height of 107 m) to 803.14 million kWh (dam height of 67 m). Considering the efficiency of the couple turbine generator as 70%, the net energy function becomes:

\[
E_{\text{net}} = E_h' - E_{\text{bio}}
\]

Table 2 Hydroenergy, thermal and net energy (million kWh) available from submerged area at Magod

<table>
<thead>
<tr>
<th>Dam height</th>
<th>Hydroenergy, (E_h)</th>
<th>Bioenergy, (E_{\text{bio}}) @6.5 t ha(^{-1}) year(^{-1})</th>
<th>Net energy (million kWh): (E_h - E_{\text{bio}})</th>
<th>(E_h - E_{\text{bio}})</th>
</tr>
</thead>
<tbody>
<tr>
<td>107</td>
<td>746.66</td>
<td>329.77</td>
<td>416.89</td>
<td>407.24</td>
</tr>
<tr>
<td>97</td>
<td>760.55</td>
<td>219.42</td>
<td>541.13</td>
<td>455.59</td>
</tr>
<tr>
<td>87</td>
<td>780.68</td>
<td>100.36</td>
<td>679.72</td>
<td>510.93</td>
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<tr>
<td>82</td>
<td>792.27</td>
<td>72.91</td>
<td>723.36</td>
<td>531.87</td>
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<tr>
<td>77</td>
<td>810.82</td>
<td>58.25</td>
<td>752.57</td>
<td>547.19</td>
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<tr>
<td>72</td>
<td>816.48</td>
<td>45.62</td>
<td>770.86</td>
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<tr>
<td>70</td>
<td>823.55</td>
<td>35.74</td>
<td>787.81</td>
<td>563.97</td>
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<tr>
<td>67</td>
<td>823.55</td>
<td>20.41</td>
<td>803.14</td>
<td>569.34</td>
</tr>
</tbody>
</table>

Note: \(E_h' = 0.7 \times E_h\)
where $Eh'$ is $0.7 Eh$. To account for only the final amount of electricity, the thermal energy content of source is discounted by the conversion efficiency of 35%. Thus:

$$E_{net} = Eh' - 0.35 E_{tho}$$ \hspace{1cm} (28)

The result of this computation is given in the last column of Table 2. It shows that variation in net available energy at Magod ranges from 407.24 to 569.34 million kWh.

The domestic fuelwood consumption survey revealed that 82–90% of households still depend on fuelwood and agricultural residues, estimated to be 312 million kWh, to meet their domestic requirements annually. Considerations of system efficiency, peak power and socio-economic factors, all rule out the possibility of electricity entirely substituting fuelwood as a source of domestic energy. This necessitates ecologically friendly options to reduce the submergence of valuable forests.

The model and subsequent quantitative analyses demonstrate that much of the land could be saved from submergence if the hydroelectric power generation capacity is adjusted according to seasonal variations in the river’s runoff. The viability of a mixed hydroelectric power and biomass generation system is shown in energy terms, which leads to a significant reduction in the total area used for power generation. Apart from this, there is scope to generate hydroelectric energy from streams in a decentralized way.

ECONOMIC ANALYSIS

Computation of costs: net loss due to forest submersion

Forests play a role, not only in the social and economic well being of the society, but also in maintaining the ecological balance. The direct costs of the submerged area are assessed by considering standing biomass in the area, which is based on species diversity studies carried out in sample plots at Sonda, Kallabe, etc. The cost of timber, fuelwood and minor forest produce works out to be in the range of $2.25–4.55$ million Rs (Indian Rupees: Rs 42 = US$1) per hectare depending on vegetation cover. In this computation, the price of forest land is taken as Rs 111 200 ha$^{-1}$. Some attempts have been made to quantify the environmental cost of the loss of a forest arriving at 1413 million Rs ha$^{-1}$ for tropical forest and 12.87 million Rs ha$^{-1}$ sub-tropical forest (Maudgal & Kakkar, 1992).

Loss due to submersion of agricultural and horticultural land

The details of villages submerged and number of households affected are obtained from government agencies such as the Village Accountant’s office. Displacement and rehabilitation costs were based on data from earlier hydroelectric projects. Economic valuation of submerged lands is done using the market value per hectare of arecanut garden: Rs 890 000, of paddy: Rs 99 000 and of coconut plantation: Rs 218 000

Annual charges on capital costs

The capital cost depends on: (a) civil construction costs (size and type of dam) and (b) cost of the generating unit, which depends on the capacity (calculated using normal
load factor of 0.5) The schedule of rates approved recently by the government has been used in computing civil and electrical costs. This calculation, carried out for different heights, is listed in Table 3. The annual capital recovery factor (annuity factor) is calculated for the total cost (civil + electrical + environmental + rehabilitation) at 12% interest for 50 years of satisfactory functioning of the power station.

### Table 3 Civil, electrical, environmental, rehabilitation costs (million Rupees) at Magod, for various heights of dam

<table>
<thead>
<tr>
<th>Dam height (m)</th>
<th>Civil + El</th>
<th>Env (land)</th>
<th>Rehabilitation</th>
<th>Env cost</th>
<th>Total cost</th>
<th>Annual expenditure</th>
</tr>
</thead>
<tbody>
<tr>
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<td>630.72</td>
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</table>

Civil + El: civil and electrical construction costs;  
Env (land): land cost due to submersion;  
Env cost: cost due to loss of environmental benefits

### Operation and maintenance (O & M) charges

Annual O & M charges are taken as 1% of the total cost of the project. The depreciation works out to be 1.80%, taking into account the life of the dam as 70 years; that of surge shafts, penstock, power house equipment, power house building and substation equipment as 50 years, and of roads, etc, as 35 years. Hence, the annual cost, $C$, is computed as:

$$C = (\text{Annuity factor} \times \text{Total cost}) + \text{O & M charges} + \text{Depreciation cost}$$  \hspace{1cm} (29)

With this annual cost and energy information, the cost per kWh of energy, has been computed in Fig. 6. It shows 40.5% reduction in cost (Rs 1.53 kWh\(^{-1}\) to Rs 0.92 kWh\(^{-1}\)) for a dam height reduction of 32.75%. If one considers electricity from water resources only, then the cost reduction is from Rs 1.53 kWh\(^{-1}\) to Rs 1.09 kWh\(^{-1}\).

### Benefits

Benefit would be the revenue accrued as a result of electricity consumption in various sectors. The percentage share of each sector, calculated considering the annual consumption pattern in Uttara Kannada district, shows that the industrial sector, with a share of 86.38%, is a major consumer, followed by the domestic sector, with a share of 10.20%. Based on tariff information provided by Karnataka Electricity Board, sector-wise revenue has been computed. The benefit, $B$, from the power project is given as:

$$B = \sum_{j=1}^{6} c_j \cdot t_j$$  \hspace{1cm} (30)

where $j = 1, \ldots, 6$ (representing various sectors) and $c_j$ and $t_j$ are electricity consumption and tariff, respectively, in Rs kWh\(^{-1}\) for sector “$j$”.
Fig. 6 Cost per kWh of electricity generated for various heights of dam

Fig. 7 Benefit–cost ratio for various environmental costs
The benefit-cost ratio, \( \frac{B}{C} \), for various dam heights, considering the following cases, is depicted in Fig 7.

The value of forest land for Cases I, II and III is Rs 37 065, Rs 111 200 and Rs 111 200 (\( + \) Rs 12 000, minor forest produce + fuelwood) per hectare, respectively. However, for cases IV, V and VI, the value of a hectare of forest land with standing biomass is Rs 2.25 million, 4.55 million and 2.25 million (\( + \) environmental value as Rs 14.13 million), respectively.

The value \( \frac{B}{C} \) is greater than 1.5 for dam heights less than 97 m in Case I, 87 m in Case II and 82 m in Case III, while for Cases IV, V and VI, \( \frac{B}{C} \) is less than 1.5 for all heights of dam. This means that, by assigning environmental values, taking all components into consideration, the hydroelectric generation through storage (for minimum submergence also) becomes a less attractive option.

**SUMMARY**

The hydroelectricity potential of streams in the Bedhi and Aghanashini river basins is estimated to be about 720 and 510 million kWh respectively. In order to reduce the submergence of prime forests, it is necessary to look for an optimal range of reservoir size and installed generation capacity, based on certain site specific factors. Quantification of the energy cost of land submergence reveals that net energy in the region (hydropower and thermal energy in the potential biomass increment), could be maximized by optimal project dimensions.

This analysis explains the upper limit on the height of the dam and therefore the area of the reservoir for the project to yield a positive net energy. Also, it is noticed that savings in land submergence could be achieved by adjusting hydroelectric generation capacity according to seasonal variation in the river runoff. By parametric optimization technique, allowing a seasonal generation ratio of 3, the submergence area saved is about 69.97% with subsequent increase in electricity generated. This is mainly due to less evaporation and seepage loss due to reduced submergence area for smaller dam heights.

Net energy analyses carried out by incorporating bioenergy lost in submergence at Magod show a gain of 63.9% for a reduction of 37.3% in dam height. Apart from the distinct reduction in submergence area, the overall reliability of a combined hydropower and thermal energy system is much higher than that of pure hydropower systems (which are very sensitive to fluctuations in rainfall).

Net energy computed for various dam heights shows that a reservoir with dam of height 67 m stores enough water to meet the region’s lean season electricity requirement and the area saved has a bio-resource potential of 319 million kWh that can cater to the domestic thermal energy demand of 312 million kWh.

The calculation of cost per kWh for various designs of the dam shows a 40.5% reduction in cost for a dam height reduction of 32.75%. The benefit to cost ratio, computed considering forest land value as Rs 111 200 ha\(^{-1}\) is greater than 1.5 for dam height less than 87 m.

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